# STRUCTURE AND WINDLOAD STUDY OUTDOOR TRANSIT DID (LRT STATIONS, OSLO)

Fully sealed vibration tested transit outdoor display

Model: NIOD700P-700, 70" Portrait, double-sided 700cd, IP65 Cross Track monitor

Excerpt
April 21, 2017



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### The 1st Chapter. SUMMARY OF STRUCTURE REVIEW

#### 1.1 SITE SUMMARY

We analyze the structural safety of an 70inch advertising board installed in Oslo subway station.

#### 1.2 STRUCTURAL REVIEW CRITERIA

Design Method	. Ultimate Strength Design Method (RC) / Allowable Stress Design (S, SRC) . Limit State Design (S, SRC)					
Applied Statute	. Building Act / Building Act Enforcement Decree					
Applied Rule	. Building Regulation / Regulation for Structure in Building					
Applied Criteria	. Korean Building Code (KBC2016) . Korean Steel Structure Design Code (KSSC-ASD03)					
Reference Criteria	. ACI 318 . AISC-ASD / AISC-LRFD / ANSI/AISC 360-05					

#### 1.3 Structure Materials Standards and Specified Strength

STEEL: KS D 3503 Rolled Steel Materials for Structure

- SS400, Fy = 235 MPa

#### 1.4 Analysis Program

- MIDAS/GEN (Frame Analysis, Design)
- MIDAS/SET (Member Design)

#### The 2nd Chapter. Review of Load

Dead Load(D.L) is considered automatically on analysis program, Live Load(L.L) is applied with 50 N/m, monitor load 1402N/m (1500N/1.07m=1402N/m) and Wind Load(W.L) is applied with 70 Pa offered by manufacturer. Also Horizontal Load is applied with 100 Pa to consider the load which man lean on the board.

Horizontal Load  $(100N/m^2x1.07m/2 = 46.7N/m) --> Applied 50N/m in this review$ 

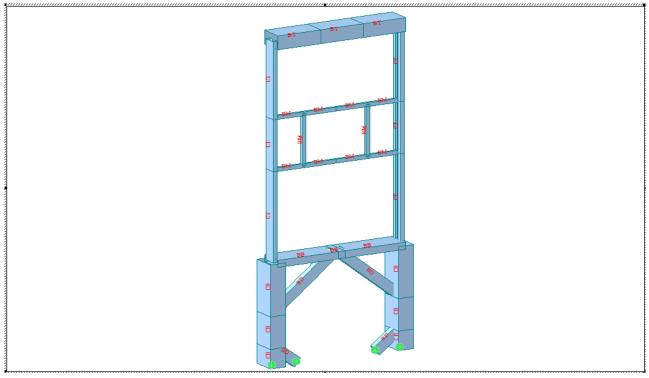
It was focused on trains passing the station without stopping. During the test most of these trains passed the station at a very low speed.

Maximum pressure from the trains was measured to approx. 70 Pa.

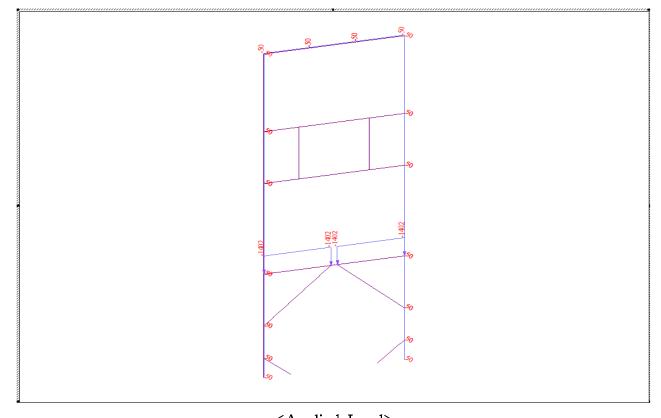
Nearly all pressure pulses measured were negative (under pressure).

LOAD COMBINATION						
1	sLCB1	D+L				
2	sLCB2	0.75(D+L+WY)				
3	sLCB3	0.75(D+L-WY)				
4	sLCB4	0.75(D+WY)				
5	sLCB5	0.75(D-WY)				

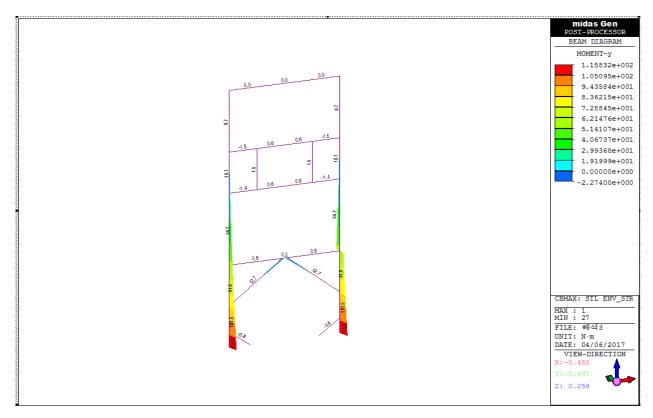
The 3rd Chapter. Structure Review



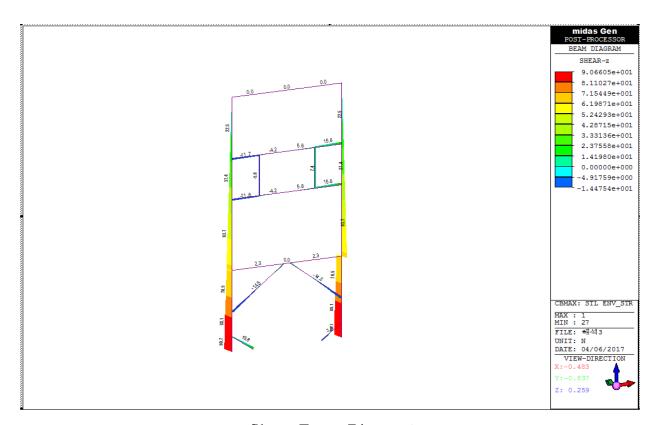




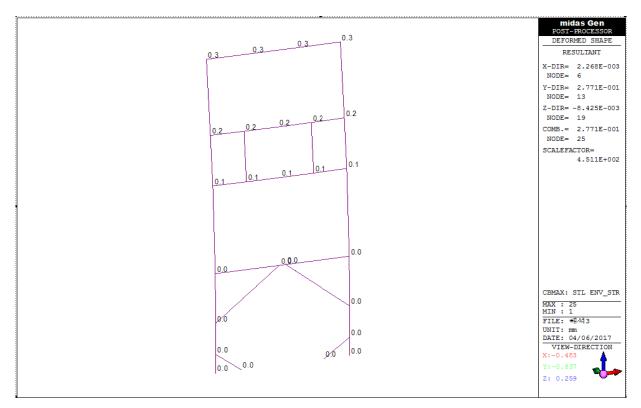
<Applied Load>



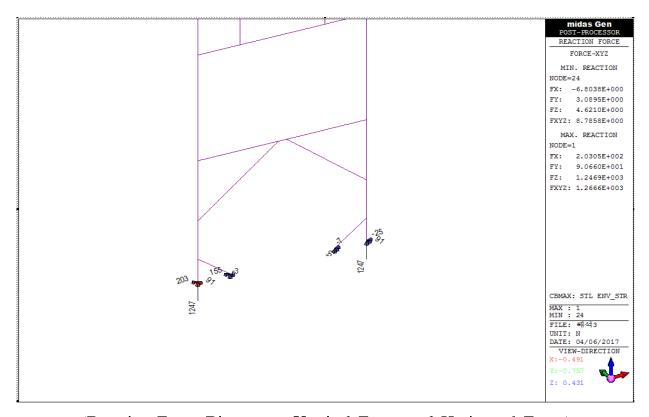
<Bending Moment Diagram>



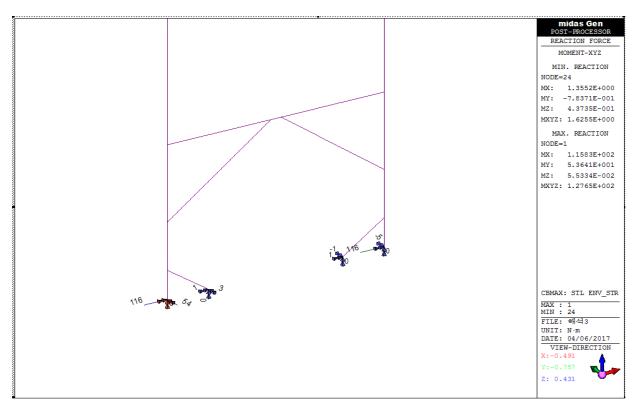
<Shear Force Diagram>



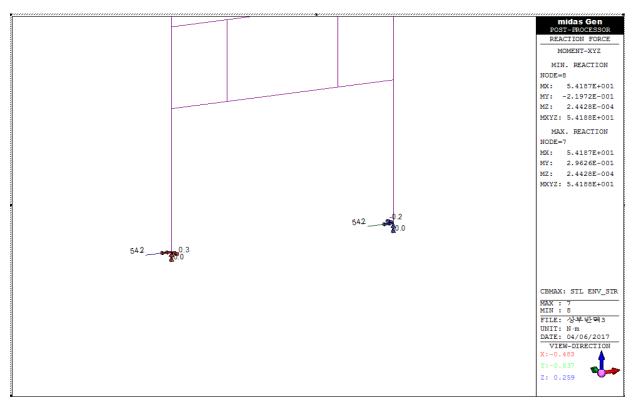
<Deformed Shape Diagram>



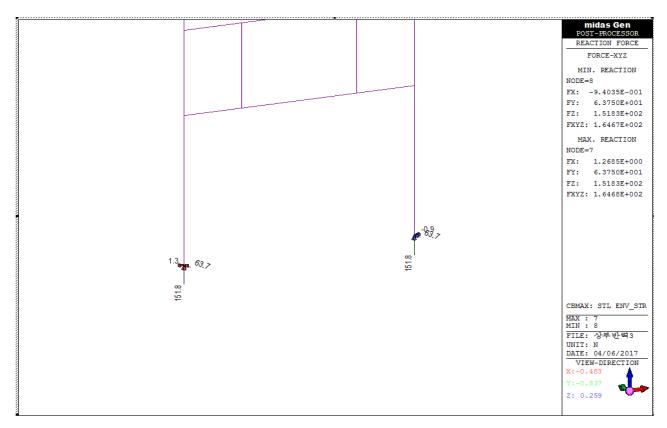
<Reaction Force Diagram - Vertical Force and Horizontal Force>



<Reaction Force Diagram - Bending Moment Diagram>



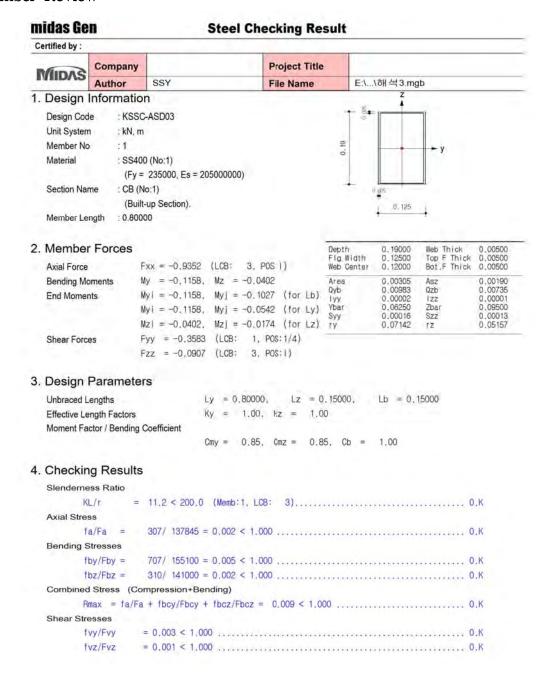
< Reaction Force Diagram of Upper Structure - Bending Moment Diagram>



< Reaction Force Diagram of Upper Structure

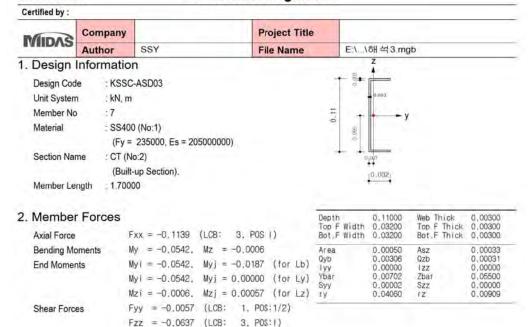
- Vertical Force and Horizontal Force>

#### 1) Member Review



#### midas Gen

#### **Steel Checking Result**



#### 3. Design Parameters

Unbraced Lengths Ly = 1.70000, Lz = 0.70000, Lb = 0.70000

Effective Length Factors Ky = 1,00, Kz = 1,00

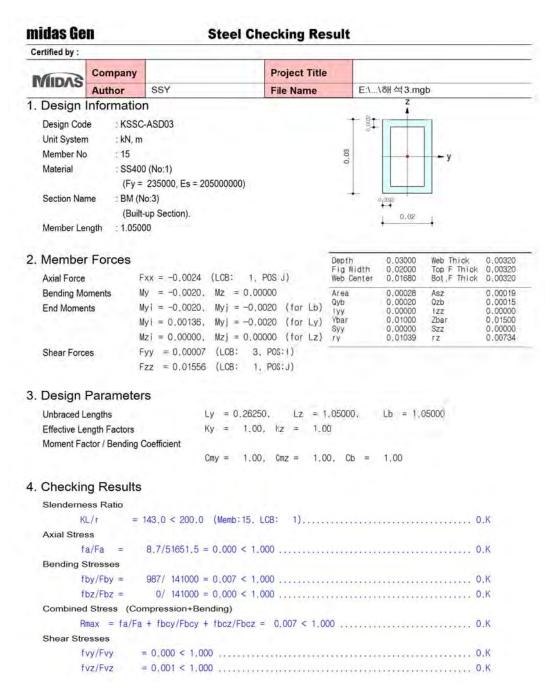
Moment Factor / Bending Coefficient

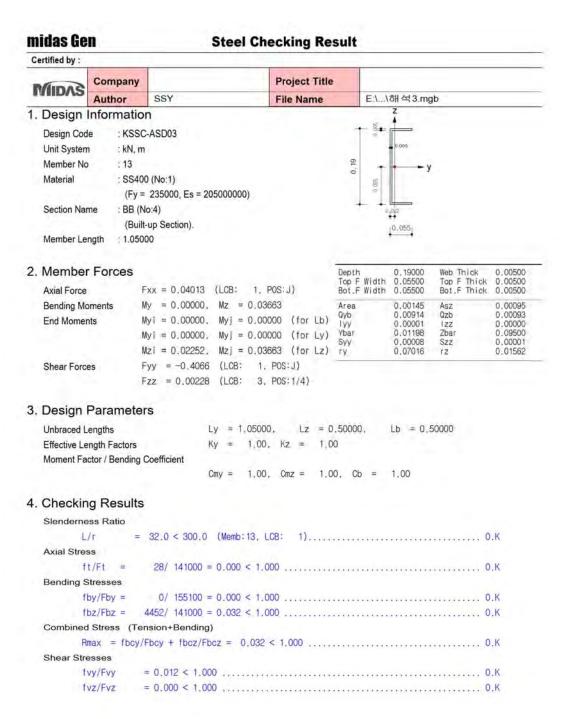
Cmy = 0.85, Cmz = 0.85, Cb = 1.00

#### 4. Checking Results

Slenderness Ratio KL/r **Axial Stress** fa/Fa 226/ 104483 = 0.002 < 1.000 ..... 0.K Bending Stresses fby/Fby = 3587/ 103481 = 0.035 < 1.000 ...... 0.K 336/ 141000 = 0.002 < 1.000 ..... 0.K fbz/Fbz = Combined Stress (Compression+Bending) Rmax = fa/Fa + fbcy/Fbcy + fbcz/Fbcz = 0.037 < 1.000 ...... 0.K Shear Stresses fvy/Fvy = 0.000 < 1.000 ..... 0.K tvz/Fvz = 0.002 < 1.000 ..... 0.K

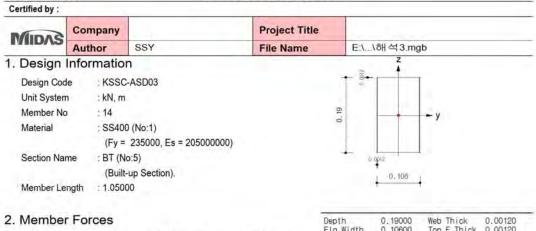
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#### midas Gen

#### **Steel Checking Result**



Axial Force	Fxx = -0.0033 (LCB: 1.	POS: 1/2)	Flg Width Web Center	0.10600 0.10480	Top F Thick Bot, F Thick	0.00120
Bending Moments	My = 0.00000, $Mz = 0.01$	330	Area	0.00070	Asz	0.00046
End Moments	Myi = 0.00000, $Myj = 0.00$	000 (for Lb)	) Cyb	0.00940	Qzb Izz	0.00632
	Myi = 0.00000, Myj = 0.00	000 (for Ly)	Ybar Syv	0.05300	Zbar Szz	0.09500
	Mzi = -0.0011. $Mzj = -0.0$	011 (for Lz)	LA	0.00004	rz.	0.04574
Shear Forces	Fyy = 0.05473 (LCB: 1.	POS:J)				
	$F_{77} = 0.00000 \text{ (LCB: 3)}$	POS: 1/2)				

#### 3. Design Parameters

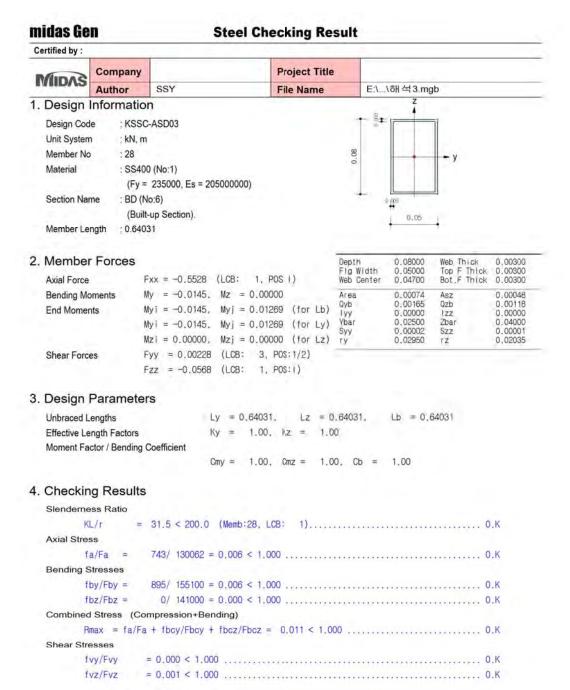
Ly = 1.05000. Lz = 1.05000. Lb = 1.05000 Unbraced Lengths Effective Length Factors 1.00. Moment Factor / Bending Coefficient

Cmy = 1.00, Cmz = 1.00, Cb =

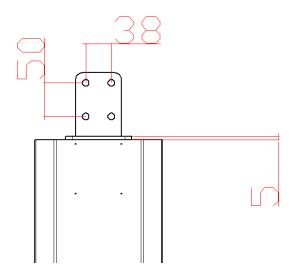
#### 4. Checking Results

#### Slenderness Ratio KL/r = 23.0 < 200.0 (Memb: 14, LCB: **Axial Stress** fa/Fa 4.6/48231.0 = 0.000 < 1.000 ..... 0.K Bending Stresses fby/Fby = 0/ 155100 = 0.000 < 1.000 ..... 0.K 1257/ 141000 = 0.009 < 1.000 ..... 0.K Combined Stress (Compression+Bending) Rmax = fa/Fa + fbcy/Fbcy + fbcz/Fbcz = 0.009 < 1.000 ...... 0.K Shear Stresses fvy/Fvy = 0.002 < 1.000 ..... 0.K fvz/Fvz = 0.000 < 1.000 ..... 0.K

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2) Connecting Bolt of Upper-Lower Member (Base+Monitor)



① Internal Force of Wrench Bolt M10

$$Vr = 9.18kN/ea$$

2 Design Load

$$M = 54.2 \text{ N.m}$$

$$Vx = 64N$$
,  $Rx = Vx/4 = 16.0N/ea$ 

$$Vy = 152N$$
,  $Ry = Vy/4 = 38.0N/ea$ 

3 Bolt Review

$$\sum (x_i^2 + y_i^2) = 4(19^2 + 25^2) = 3944$$

$$R_{m,x} = \frac{M \times y_m}{\sum (x^2 + y^2)} = \frac{54.2 \times 1000 \times 25}{3944} = 344 \text{N/ea}$$

$$R_{m,y} = \frac{M \times x_m}{\sum (x^2 + y^2)} = \frac{54.2 \times 1000 \times 19}{3944} = 261 \text{N/ea}$$

$$R = \sqrt{(R_{m,x} + V_x)^2 + (R_{m,y} + V_y)^2} = \sqrt{(344 + 16.0)^2 + (261 + 38.0)^2} = 468N/ea$$

3) Connectiong Bolt of Foundation Member



① Internal Force of Hilti HVU-HAS M16 (Refer to Hilti Manual)

Fz,r = 24.8kN

Fx,r = 24.7kN

2 Design Load

M = 116 N.m

Fz = 1247N

Vx = 203N

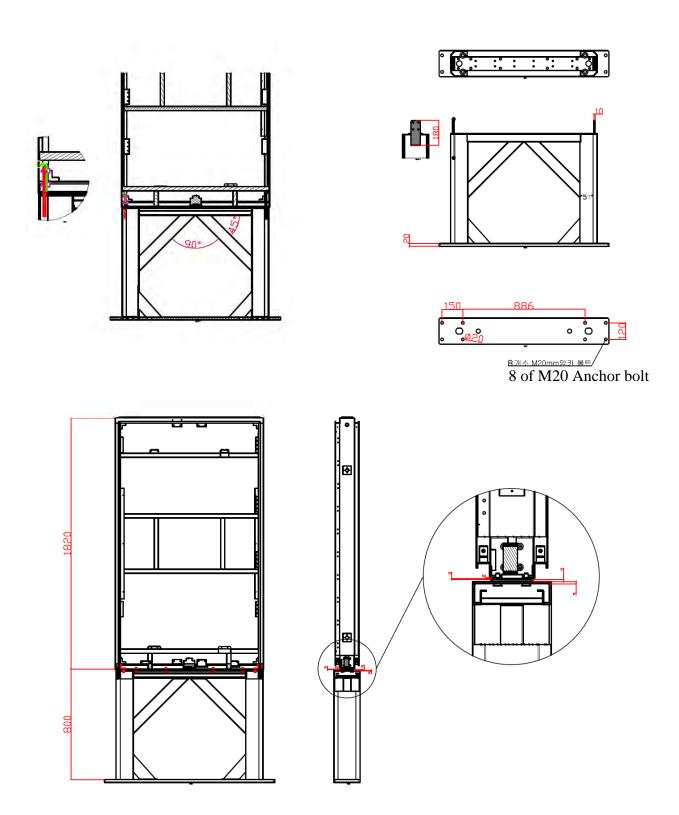
Vy = 92N

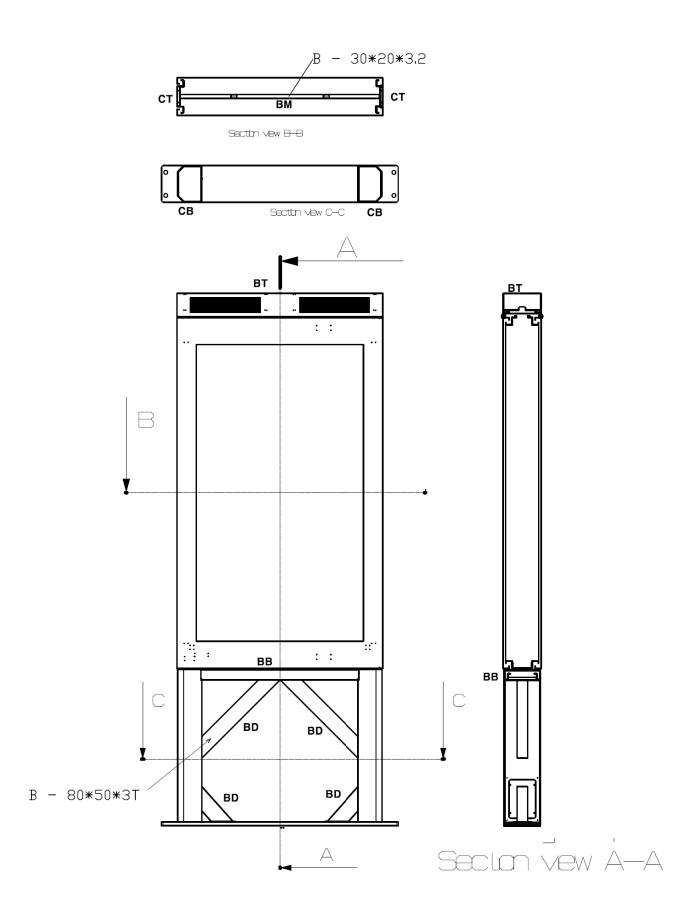
3 Axial Force Review

M/d+Fz = 116/0.12+1247 = 967+1247 = 2214N < Fz,r = 24.8kN ----> O.K

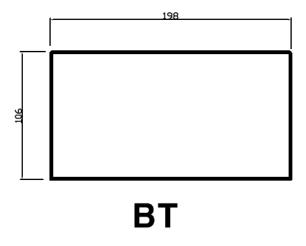
4 Shear Force Review

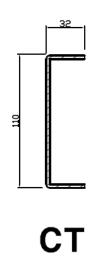
 $V = (Vx^2+Vy^2)^{0.5} = 223N < Fx,r = 24.7kN$  ----> O.K

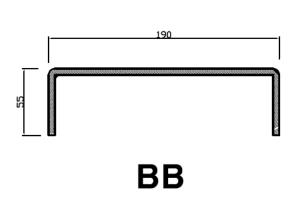


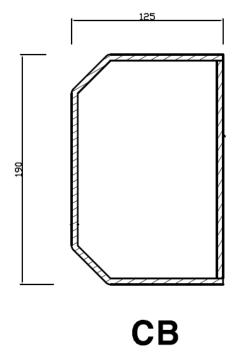


## **Approximative Member Section**









#### The 5th Chapter. Review Result

1) The 70inch advertising board installed in Oslo subway station secured structural safety on dead load and 100 Pa of wind load in subway station and leaning load, if it is installed as reviewed drawing.

This is to confirm that model #NIOD-700P, 70" Double-sided transit KIOSK, is structurally safe on dead load and 100 Pa of wind load in subway station at Oslo subway station as reviewed drawing.